

TITLE OF THE INVENTION  
EXPOSURE APPARATUS AND DEVICE MANUFACTURING  
METHOD USING THE SAME

5 FIELD OF THE INVENTION

The present invention relates to an exposure apparatus used in the lithography step of the steps in manufacturing a device, e.g., a semiconductor device such as an IC or LSI, a liquid crystal device, an image  
10 sensing device such as a CCD, or a magnetic head, and a device manufacturing method using the exposure apparatus.

BACKGROUND OF THE INVENTION

15 In a manufacturing process of a semiconductor integrated circuit, an exposure apparatus is used to form a pattern on a photosensitive material (to be referred to as a "resist" hereinafter) on a substrate (to be referred to as a "wafer" hereinafter). With an  
20 increase in the area of recent semiconductor integrated circuits and an advance in micropatterning, a scanning exposure apparatus called a step-and-scan exposure apparatus designed to illuminate part of a pattern on a mask as a master in the form of a slit, and perform  
25 exposure by synchronously scanning the mask and a wafer at a constant velocity is replacing a conventional step-and-repeat exposure apparatus, a so-called stepper,

which is designed for cell projection of a mask pattern.

In general, a proper exposure amount (to be referred to as a "set exposure amount" hereinafter)  $D$  ( $J/m^2$ ) for the formation of a proper mask pattern image is set for a resist. A scanning velocity  $V$  (mm/sec) in the scanning exposure apparatus must satisfy

$$V \leq I_{\max}/D \times W_s \quad \dots(1)$$

where  $I_{\max}$  ( $W/m^2$ ) is the maximum exposure illuminance of exposure light on a wafer, and  $W_s$  (mm) is the exposure slit width on the wafer in a non-scanning direction.

According to inequality (1), the maximum scanning velocity controlled by the set exposure amount  $D$  is given by

$$V_d = I_{\max}/D \times W_s \quad \dots(2)$$

A maximum scanning velocity  $V_{\max}$  determined from the performance of a stage control system, including structural/mechanical performance, is substantially determined in the scanning exposure apparatus, and the scanning velocity  $V$  must satisfy

$$V \leq V_{\max} \quad \dots(3)$$

One of the factors responsible for the above requirement is that the positions of a mask and wafer cannot be properly controlled to result in a deviation (to be referred to as a "synchronization error" hereinafter), i.e., a deviation from a predetermined

positional relationship between the mask and the wafer,  
in the scanning exposure apparatus designed to form a  
mask pattern on the wafer by scanning/exposing the mask  
and wafer while performing synchronous control to keep  
5 the positions of the mask and wafer in the  
predetermined positional relationship. This leads to a  
decrease in the resolution of a resist pattern and a  
deviation from the proper imaging position of the  
resist pattern, resulting in a trouble in the  
10 manufacture of a semiconductor integrated circuit.  
This synchronization error is almost proportional to  
the scanning velocity. As the scanning velocity  
increases, the synchronization error increases. For  
this reason, the maximum scanning velocity  $V_{max}$  that  
15 suppresses the synchronization error within an  
allowable synchronization error range is determined.

If a pulsed light source such as a KrF excimer  
laser or ArF excimer laser is used as an exposure light  
source to meet the requirement for micropatterning,  
20 since pulsed light varies in energy for each pulse, an  
integrated exposure amount is made uniform within a  
desired precision by performing exposure with a  
plurality of pulsed light beams equal to or larger than  
a predetermined pulse count (to be referred to as a  
25 "minimum exposure pulse count" hereinafter)  $P_{min}$ . For  
this reason, in the scanning exposure apparatus, the  
following inequality must be satisfied:

$$P_{min} \leq W_s/V \times f \quad \dots(4)$$

where  $f$  (Hz) is the oscillation frequency of the exposure light source laser.

According to inequality, letting  $f_{max}$  be the maximum oscillation frequency of the exposure light source laser, the maximum scanning velocity controlled by the minimum exposure pulse count  $P_{min}$  is given by

$$V_p = W_s/P_{min} \times f_{max} \quad \dots(5)$$

Conventionally, as disclosed in, for example, Japanese Patent Laid-Open Nos. 10-270345 and 10-223513, a scanning velocity is determined with the oscillation frequency  $f_{max}$  when a low-sensitivity resist with the large set exposure amount  $D$  is to be used, or a scanning velocity is determined to set the maximum scanning velocity  $V_{max}$  when a high-sensitivity resist with the small set exposure amount  $D$  is to be used, so as to satisfy inequalities (1), (3), and (4).

If the integrated exposure amount can be set to  $P_{min}$  regardless of the maximum scanning velocity  $V_d$  controlled by the set exposure amount  $D$  represented by equation (2), the maximum scanning velocity  $V_{max}$  controlled in accordance with the performance of the apparatus, and the value of the set exposure amount  $D$ , the minimum value of  $V_p$  controlled by the minimum exposure pulse count represented by equation (5) is determined as a scanning velocity in actual exposure operation.



possible scanning velocity of the maximum scanning velocities  $V_d$ ,  $V_{max}$ , and  $V_p$ .

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This indicates that the throughput increases as the scanning velocity increases. Obviously, in a scanning exposure apparatus designed to illuminate a pattern area to be exposed in the form of a slit and perform exposure by synchronously scanning a mask and wafer at a constant velocity, the time required to scan the pattern area to be exposed shortens as the scanning velocity increases while the length of the pattern area to be exposed in the scanning direction remains unchanged.

However, after one pattern area is exposed, both the mask stage and the wafer stage are temporarily stopped. Thereafter, the next pattern area is exposed by scanning the stages in the opposite direction. To increase the mask and wafer scanning velocities, therefore, is to prolong the time required to accelerate each scanning velocity to the above scanning velocity and the time required to decelerate each of the mask and wafer scanning velocities to 0. At a given scanning velocity or higher, since the time required to scan a pattern area to be exposed shortens because of an increase in scanning velocity. However, the time required to accelerate each of the mask and wafer scanning velocities to the scanning velocity in the pattern area to be exposed and the time required to

decelerate each scanning velocity to 0 is prolonged more than the time shortened. As a result, the total time required to start driving a mask and wafer, reach the scanning velocity in a pattern area to be exposed, and complete driving operation of the mask and wafer may be prolonged as the scanning velocity is increased, resulting in a reduction in throughput.

#### SUMMARY OF THE INVENTION

The present invention has been made in consideration of the above points, and has as its object to provide an exposure apparatus which has a scanning velocity determination means to maximize the throughput.

In order to achieve the above object, according to the present invention, there is provided a scanning exposure apparatus comprising: a master stage for scanning a master, a substrate stage for scanning a substrate, transfer means for supplying/recovering the substrate to/from the substrate stage, and positioning means for relatively positioning the substrate and the master, scanning velocity determination means for determining a scanning velocity so as to maximize the number of substrates that can be exposed per unit time, i.e., a throughput.

The scanning velocity determining means determines, as a scanning velocity in actual exposure

operation, a lowest one of

a maximum scanning velocity determined from  
apparatus performance:  $V_{max}$ ,

a scanning velocity determined from an exposure  
5 illuminance and a required exposure amount:  $V_d$ , and

a scanning velocity at which the number of  
substrates that can be processed per unit time is  
maximized, which is determined from the transfer  
pattern size, a layout of the transfer pattern on the  
10 substrate, the transfer means, the master scanning  
means, the substrate stage scanning means, and the  
positioning means:  $V_t$ .

If the light source is a light source for  
emitting pulsed light, the scanning velocity  
15 determining means determines, as a scanning velocity in  
actual exposure operation, a lowest one of

a maximum scanning velocity determined from  
apparatus performance:  $V_{max}$ ,

a scanning velocity determined from an exposure  
20 illuminance and a required exposure amount:  $V_d$ ,

a scanning velocity determined from the minimum  
number of pulses which is required for integration to  
ensure a uniform exposure amount:  $V_p$ , and

a scanning velocity at which the number of  
25 substrates that can be processed per unit time is  
maximized, which is determined from the transfer  
pattern size, a layout of the transfer pattern on the



substrate, the transfer means, the master scanning means, the substrate stage scanning means, and the positioning means:  $V_t$ .

More specifically, the scanning velocity  $V_p$   
5 satisfies

$$V_p = W_s / P_{min} \times f_{max}$$

where  $W_s$  is a width of an illumination area, on the substrate in a non-scanning direction, which illuminates part of the transfer pattern,  $f_{max}$  is a  
10 maximum frequency of pulsed light emitted from the light source, and  $P_{min}$  is the minimum number of pulses required for integration to ensure a uniform exposure amount on the substrate.

The scanning velocity  $V_d$  satisfies

15 
$$V_d = I_{max} / D \times W_s$$

where  $I_{max}$  is a maximum exposure illuminance, and  $D$  is a required exposure amount determined by a photosensitive material.

The scanning velocity  $V_t$  is calculated by  
20 simulation to maximize the number of substrates that can be processed per unit time on the basis of the transfer pattern size, a layout of the transfer pattern on the substrate, and conditions in the master scanning means, the substrate stage scanning means, the transfer  
25 means, and the positioning means or satisfies

$$V_{scan.min} = \sqrt{\{L \times \alpha_{accel} \times \alpha_{decel} / (\alpha_{accel} + \alpha_{decel})\}}$$

$$V_t = g(V_{\text{scan.min}})$$

where  $\alpha_{\text{accel}}$  is an average acceleration with which an increase in scanning velocity from 0 to  $V_t$  is achieved,  $\alpha_{\text{decel}}$  with which a decrease in scanning velocity from  $V_t$  to 0 is achieved,  $L$  is a length on the substrate which is scanned at a constant velocity in one scanning operation, and  $g()$  is an arbitrary function.

In this case, since the length  $L$  changes for each transfer pattern in accordance with the transfer pattern size and the layout of the transfer pattern on the substrate, the optimal value of  $V_t$  is determined to be changed for each transfer pattern. In addition, the scanning velocity  $V_t$  may be changed for each shot area to be exposed in accordance with the length that is scanned at a constant velocity in one scanning operation.

By determining a scanning velocity in this manner, a maximum throughput can always be obtained, and hence the productivity of devices can be increased.

Other features and advantages of the present invention will be apparent from the following description taken in conjunction with the accompanying drawings, in which like reference characters designate the same or similar parts throughout the figures thereof.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic view showing the arrangement of an exposure apparatus according to an embodiment of the present invention;

Fig. 2 is a view for explaining a shot area and exposure slit in scanning exposure;

Fig. 3A is a view for explaining a shot layout on a wafer and an exposure order in an exposure apparatus according to the first embodiment of the present invention;

Fig. 3B is a view for explaining a shot layout on a wafer and an exposure order in an exposure apparatus according to the second embodiment of the present invention;

Fig. 4 is a chart showing the relationship between the wafer stage velocity and the time in scanning exposure according to the first embodiment of the present invention;

Fig. 5 is a chart showing the relationship between the wafer stage velocity and the time in scanning exposure according to the second embodiment of the present invention;

Fig. 6A is a graph for explaining a stage acceleration pattern;

Fig. 6B is a graph for explaining a stage acceleration pattern;

Fig. 7A is a graph showing the relationship between the scanning velocity and the throughput;

Fig. 7B is a graph showing the relationship between the scanning velocity and the time period from the start of scanning of a shot area to the end of scanning;

5 Fig. 7C is a graph showing the relationship between the scanning velocity and the time period from the start of scanning of a shot area to the end of scanning;

Fig. 8 is a view showing the concept of a  
10 semiconductor device production system according to the present invention when viewed from a given angle;

Fig. 9 is a view showing the concept of the semiconductor device production system according to the present invention when viewed from another given angle;

15 Fig. 10 is a view showing an example of a user interface in the exposure apparatus according to the present invention;

Fig. 11 is a flow chart showing the flow of a semiconductor device manufacturing process according to  
20 the present invention; and

Fig. 12 is a flow chart showing a wafer process in Fig. 11 which is performed by the exposure apparatus according to an embodiment of the present invention.

25 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS  
(First Embodiment)

Fig. 1 is a schematic view showing an exposure

apparatus according to an embodiment of the present invention. In this case, a pulse laser such as an excimer laser is used as an exposure light source. A light beam L emitted from a light source 1 formed by a pulse laser such as an excimer laser is shaped into a predetermined shape by a beam shaping optical system 2 and incident on an optical integrator 3. The optical integrator 3 is formed by a flyeye lens constituted by a plurality of microlenses, and has a plurality of secondary sources near its light exit surface. Light beams from the secondary sources near the light exit surface of the optical integrator 3 illuminate, through a condenser lens 4, a movable slit 6 whose aperture shape can be changed. Reference numeral 14 denotes an exposure amount detector A for detecting the amount of part of illumination light split by a half mirror 5 and outputting the resultant signal to an exposure amount computing unit 102.

The light beams illuminating the movable slit 6 illuminate part of a circuit pattern, in the form of a slit, which is formed on a mask 10 serving as a master held on a mask stage 9, through an imaging lens 7 and mirror 8.

With a light beam in the form of a slit, which has passed through the mask 10, the circuit pattern on the mask 10 is reduced/projected, through a projection lens 11, on a wafer 12 having a surface coated with a

resist as a photosensitive material. The wafer 12  
serving as a substrate to be exposed is held on a wafer  
stage 13 that can be driven in the X, Y, and Z  
directions and tilt direction. An exposure amount  
5 detector B (15) is mounted on the wafer stage 13 to  
monitor an exposure amount through the projection lens  
11. At an early stage in an exposure process, the  
correlation between the amount of exposure light that  
has passed through the projection lens 11 and detected  
10 by the exposure amount detector B (15) on the wafer  
stage 13 and the amount of exposure light that is  
detected by the exposure amount detector A (14) is  
obtained in advance, and actual exposure operation is  
controlled on the basis of the exposure amount detected  
15 by the exposure amount detector A (14).

Reference numeral 101 denotes a laser control  
system for controlling the output energy and  
oscillation frequency of the light source 1 by  
outputting a trigger signal and charging voltage signal  
20 in accordance with a desired set exposure amount. This  
apparatus includes a light attenuation means (not  
shown) and can adjust the amount of light from the  
light source 1.

The positions of the mask stage 9 and wafer stage  
25 13 are respectively measured by interferometers 16 and  
17, and a mask stage control system 104 and wafer stage  
control system 105 respectively control the mask stage

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9 and wafer stage 13 in accordance with an instruction from a main control system 103 to accurately scan the light beam that illuminates part of the mask pattern in the form of a slit in opposite directions at  
5 predetermined velocities at a ratio equal to a projection magnification  $\beta$  of the projection lens 11. In this manner, as shown in Fig. 2, the slit-like light beam continuously scans/exposes an entire exposure area (to be referred to as a "shot area" hereinafter) on the  
10 wafer 12 exposed to a mask pattern, thus exposing/transferring the entire mask pattern onto the wafer 12. Referring to Fig. 2, each hatched portion e is a portion of the wafer 12 that is actually exposed, and each dotted portion s indicates the slit. The  
15 movement of a light beam between the respective shot areas on the wafer 12 is performed by XY-driving the wafer stage 13.

After all desired shot areas on the wafer 12 are completely exposed, the wafer 12 is transferred outside  
20 the exposure apparatus from the wafer stage 13 through a wafer recovery/transfer system 18. At the same time, the next wafer is supplied onto the wafer stage 13 via a wafer supply/transfer system 19 (identical to the wafer recovery/transfer system 18 in Fig. 1 for the  
25 sake of illustrative convenience). Thereafter, an alignment system (not shown) performs positioning with the pattern that has already been formed on the wafer

12. According to one alignment method, the positions of alignment marks mainly formed on peripheral portions of a plurality of shot areas selected on the wafer 12 to obtain rotation, expansion/contraction, and shift offsets and the like of the wafer 12, thereby positioning all shot areas on the wafer 12. Coarse alignment for the detection of alignment marks is sometimes performed before this fine alignment. After each shot area is positioned in this manner, the above exposure operation is repeatedly performed.

A procedure for obtaining a scanning velocity at which a maximum throughput can be obtained will be described next.

A "throughput" will indicate the number of wafers exposed by the apparatus per unit time under a proper exposure under conditions for proper exposure hereinafter. The "number of wafers processed" to be described later indicates the number of wafers processed by the apparatus per unit time regardless of whether conditions for proper exposure are set or not.

First, in a scanning exposure apparatus, a maximum scanning velocity  $V_{max}$  is substantially determined, which is determined from the performance of a system control system, including structure and mechanical performance, in order to attain desired imaging performance and overlay accuracy. That is, if scanning exposure is performed at this velocity or



higher, a desired fine integrated circuit pattern cannot be formed or a desired overlay accuracy cannot be ensured. Therefore, a scanning velocity V must satisfy

5  $V \leq V_{\max}$  ... (6)

Second, a proper exposure amount D is determined depending on the type of resist to be used and an exposure process to properly form a circuit pattern on the mask 10. In scanning exposure, exposure amount control is performed to set the exposure amount at each point on the wafer 12 to the above proper exposure amount D. Letting I<sub>max</sub> be the maximum exposure illuminance in scanning exposure and W<sub>s</sub> be the slit width on the wafer 12 in the scanning direction, the scanning velocity V must satisfy

$V_d = I_{\max}/D \times W_s$  ... (7)

$V \leq V_d$  ... (8)

If the scanning velocity V must be set to be lower than V<sub>d</sub>, the illuminance must be decreased. As methods of decreasing the illuminance, for example, the following methods are available: a method of decreasing the illuminance by decreasing the energy per laser pulse; a method of decreasing the illuminance by attenuating pulsed light by using a light attenuation means such as an ND filter set on an optical path; a method of decreasing the illuminance by decreasing the pulse oscillation frequency; and a combination of these

methods.

Third, with a reduction in the size of an IC pattern, the illuminance evenness of exposure light is required for the performance of the exposure apparatus.

5 However, pulsed light from a pulsed light source such as an excimer laser varies in energy for each pulse. For this reason, exposure must be performed with the number of pulses equal to or more than a predetermined pulse count  $P_{min}$  at each point on a wafer to integrate  
10 pulse energy so as to maintain predetermined illuminance evenness.

Letting  $f_{max}$  be the maximum oscillation frequency of the exposure light source, therefore, the scanning velocity  $V$  must satisfy

15 
$$V_p = W_s / P_{min} \times f_{max} \quad \dots (9)$$

$$V \leq V_p \quad \dots (10)$$

Fourth, without any consideration given to the first to third conditions, letting  $V_t$  be the maximum scanning velocity at which the number of wafers that  
20 can be processed by the apparatus per unit time (to be referred to as "the number of wafers processed" hereinafter) is maximized, in order to prevent a decrease in throughput, the scanning velocity  $V$  must satisfy

25 
$$V \leq V_t \quad \dots (11)$$

The above scanning velocity  $V_t$  will be described next.

Letting  $T$  (sec) be the time required to process one wafer, the number  $N$  of wafers processed per unit time is defined by

$$N = 3600/T \quad \dots(12)$$

5        An example of a breakdown of the time  $T$  required to process one wafer can be expressed as follows.

Letting  $T_{load}$  (sec) be the time required to supply a wafer,  $T_{align}$  (sec) be the time required for alignment,  $T_{scan}$  (sec) be the time required for scanning exposure, 10 and  $T_{unload}$  (sec) be the time required to recover the wafer, then the time  $T$  is defined by

$$T = T_{load} + T_{align} + T_{scan} + T_{unload} \quad \dots(13)$$

$T_{load}$ ,  $T_{align}$ ,  $T_{scan}$ , and  $T_{unload}$  are the functions of the wafer stage velocity and acceleration, 15 shot size, shot layout, and the like and can be expressed as follows:

$$T_{load} = T_{load}(V_{sl}, \alpha_{sl}, \dots)$$

$$T_{align} = T_{align}(V_{sa}, \alpha_{sa}, \text{Layout\_align}, V_{scan}, \alpha_{scan}, \dots)$$

20         $T_{scan} = T_{scan}(V_{scan}, \alpha_{scan}, V_{step}, \alpha_{step}, \text{layout\_shot}, \text{Size\_shot}, \dots)$

$$T_{unload} = T_{unload}(V_{sul}, \alpha_{sul}, \text{Layout\_shot}, V_{scan}, \alpha_{scan}, \dots)$$

$$T = T_{load} + T_{align} + T_{scan} + T_{unload}$$

25        where

$V_{sl}$  (mm/sec): wafer stage velocity in supplying wafer

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$\alpha_{sl}$  (mm/sec<sup>2</sup>): wafer stage acceleration in  
supplying wafer  
 $V_{sa}$  (mm/sec): wafer stage velocity during  
alignment  
5  $\alpha_{sa}$  (mm/sec<sup>2</sup>): wafer stage acceleration during  
alignment  
 $Layout\_align$ : layout at alignment mark  
measurement position  
 $V_{scan}$  (mm/sec): wafer stage/mask stage velocity  
10 during scanning exposure  
 $\alpha_{scan}$  (mm/sec<sup>2</sup>): wafer stage/mask stage  
acceleration during scanning  
exposure  
 $V_{step}$  (mm/sec): wafer stage velocity during  
15 movement of shot area  
 $\alpha_{step}$  (mm/sec<sup>2</sup>): wafer stage acceleration  
during movement of shot area  
 $Layout\_shot$ : shot layout  
 $Size\_shot$ : size of shot area  
20  $V_{ul}$  (mm/sec): wafer stage velocity in wafer  
recovery  
 $\alpha_{ul}$  (mm/sec<sup>2</sup>): wafer stage acceleration in wafer  
recovery

For the sake of simplicity, the communication  
25 time and computation time required for software to  
control driving of the wafer stage 13, mask stage 9,  
and the like, alignment mark measurement time, and the

like are omitted, and each velocity and acceleration  
are written without discrimination between the wafer  
stage 13 and the mask stage 9, and between scanning  
direction, non-scanning direction, accelerating  
5 operation, decelerating operation, and the like.

The reason why Talign is a function of the  
scanning velocity Vscan and scanning acceleration  $\alpha$   
scan is that movement from the final shot in alignment  
to the scanning start position for the first exposure  
10 shot is included. The scanning start position is a  
position spaced apart from a shot area to be exposed by  
an acceleration distance required to reach a desired  
scanning velocity. Scanning of the wafer stage 13 is  
started from this position. If, therefore, the  
15 scanning acceleration  $\alpha$ scan remains the same, the  
acceleration distance required to reach the scanning  
velocity Vscan decreases as the scanning acceleration  
Vscan decreases, and vice versa. Since the moving  
distance from the alignment final measurement position  
20 to the first exposure shot start position changes, the  
moving time also changes. For this reason, Talign is a  
function of the scanning velocity Vscan and scanning  
acceleration  $\alpha$ scan. Likewise, the reason why Tunload  
is a function of the scanning velocity Vscan and  
25 scanning acceleration  $\alpha$ scan is that movement from the  
scanning exposure end position in the final shot to the  
wafer recovery position is included.

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As the wafer stage velocity and acceleration in supplying a wafer, the maximum values in terms of the capacity of the apparatus are used to minimize the time Tload required to supply the wafer. The time Tload  
5 remains constant regardless of the scanning velocity Vscan. As the wafer stage velocity and acceleration during alignment, the maximum values in terms of the capacity of the apparatus are used to minimize the time Talign required for alignment. Strictly speaking,  
10 although Talign is a function of the scanning velocity Vscan, since alignment is performed by sequentially measuring alignment marks in a plurality of shot areas, the difference between the scanning velocity Vscan and the scanning acceleration  $\alpha_{scan}$  has little influence  
15 on the time Talign. Hence, this time can substantially be regarded as a constant value regardless of the scanning velocity Vscan. In addition, the time Tunload required for wafer recovery is also a function of the scanning velocity Vscan. Likewise, this time can  
20 substantially be regarded as a constant value regardless of Vscan.

Therefore, the number N of wafers processed per unit time is substantially determined by the time Tscan required for scanning exposure.

25 The relationship between the time required for scanning exposure, the wafer stage velocity, and the mask stage velocity will be described next with

reference to Figs. 3A and 4.

Fig. 3A schematically shows the layout of shot areas. Each arrow indicates the scanning route of the slit. The exposure order is  $S \rightarrow A \rightarrow B \rightarrow C \rightarrow \dots$ . The slit is relatively scanned upward in a shot area A and downward in a shot area B.

Fig. 4 shows an example of the relationship between the time, the wafer stage velocity, and the mask stage velocity. In this case, the scanning direction coincides with the Y-axis, and the non-scanning direction coincides with the X-axis. Referring to Fig. 4, the upper, intermediate, and lower charts schematically show the relationships between the velocity of the wafer stage 13 in the Y-axis direction and the time, between the velocity of the wafer stage 13 in the X-axis direction and the time, and between the velocity of the mask stage 9 in the Y-axis direction and the time, respectively.

The wafer stage 13 starts to accelerate from a velocity of 0 at time  $t_{A0}$  with an average acceleration  $\alpha_{\text{accel}}$ , and reaches the scanning velocity  $V_{\text{scan}}$  at time  $t_{A1}$ . Then, after a lapse of a time  $t_{\text{settle}}$  required to settle the synchronization error between the wafer stage 13 and the mask stage 9 within a predetermined precision range, exposure is started at time  $t_{A2}$ . The distance that the wafer stage 13 travels until this exposure start time is considered in

advance as an approach distance to set the position of the wafer stage 13 at time  $t_{A0}$ . As shown in Fig. 2, a distance  $L$  required for scanning an entire shot area at a constant velocity is the sum of a length  $L_y$  of the shot area in the scanning direction and the length  $W_s$  of the slit in the scanning direction. The exposure time is therefore given by  $L/V_{scan} = (L_y + W_s)/V_{scan}$ . The exposure ends at time  $t_{A3}$ . The wafer stage 13 then starts decelerating with an average acceleration  $\alpha_{decel}$ , and reaches the velocity 0 at time  $t_{A4}$ . Thereafter, the wafer stage 13 starts driving toward an approach start position for exposure of the shot area B. At time  $t_{A6} (= t_{B0})$ , this driving operation ends.

With regard to the non-scanning direction, the wafer stage 13 starts driving by a length  $L_x$  of the shot area in the non-scanning direction at time  $t_{A3}$  at which the exposure is terminated. At time  $t_{A5}$ , this driving operation ends. For the sake of simplicity, assume that time  $t_{A5}$  is earlier than an exposure start time  $t_{B2}$  for the shot area B. The mask stage 9 also starts decelerating at time  $t_{A0}$ , like the wafer stage 13, and reaches the velocity 0 at time  $t_{A4}$ . However, a scanning velocity  $V_{scan} (R)$  of the mask stage 9 differs from that of the wafer stage 13 by the projection magnification  $\beta$ .

Similarly, it takes the time period between time  $t_{B0}$  and time  $t_{B6}$  to expose the shot area B; and the



time period between time  $t_{C0}$  and time  $t_{C6}$  to expose a shot area C.

In this case, the step times in the scanning direction between  $t_{A4}$  and  $t_{A6}$ ,  $t_{B4}$  and  $t_{B6}$ , and  $t_{C4}$  and  $t_{C6}$ , and the step times in the non-scanning direction between  $t_{A3}$  and  $t_{A5}$ , and  $t_{B3}$  and  $t_{B5}$  are determined regardless of the scanning velocity  $V_{scan}$  as long as a shot layout and scanning order are determined.

The time period between scanning start time  $t_{A0}$  and scanning end time  $t_{A4}$  is expressed as follows:

$$t_{A1} - t_{A0} = V_{scan}/\alpha_{accel}$$

$$t_{A2} - t_{A0} = V_{scan}/\alpha_{accel} + t_{settle}$$

$$t_{A3} - t_{A0} = V_{scan}/\alpha_{accel} + t_{settle} + L/V_{scan}$$

$$t_{A4} - t_{A0} = V_{scan}/\alpha_{accel} + t_{settle} + L/V_{scan}$$

$$+ V_{scan}/\alpha_{decel}$$

Therefore, a time period  $t_{scan}(V_{scan})$  from the start of scanning of a shot area to the end of scanning is given by

$$t_{scan}(V_{scan}) = V_{scan}/\alpha_{accel} + t_{settle} + L/V_{scan} + V_{scan}/\alpha_{decel} \quad \dots (14)$$

Since the accelerations  $\alpha_{accel}$  and  $\alpha_{decel}$  take the maximum values in terms of the capacity of the apparatus to shorten the acceleration and deceleration times, these values can be regarded as constant values. Differential of second order taking  $V_{scan}$  as a variable is expressed as follows:

$$\partial^2 t / \partial V_{scan}^2 = 2 \times L/V^3 \geq 0$$

Therefore,  $t_{scan}(V_{scan})$  is a function exhibiting a characteristic in an inverted convex form, and takes a minimum value. A scanning velocity  $V_{scan.min}$  that minimizes the time period from the start of scanning of  
5 a shot area to the end of scanning is given by

$$V_{scan.min} = \sqrt{\{L \times \alpha_{accel} \times \alpha_{decel} / (\alpha_{accel} + \alpha_{decel})\}}$$

Letting  $T_{step}$  be the sum of the step times in the scanning direction between  $t_{A4}$  and  $t_{A6}$ ,  $t_{B4}$  and  $t_{B6}$ ,  
10  $t_{C4}$  and  $t_{C6}$ , ..., and  $N_{shot}$  be the number of shot areas per wafer, the time  $T_{scan}$  required for scanning exposure is given by

$$T_{scan} = T_{step} + N_{shot} \times t_{scan}(V_{scan})$$

The time  $T$  required to process one wafer is given  
15 by

$$\begin{aligned} T &= T_{load} + T_{align} + T_{scan} + T_{unload} \\ &= T_{load} + T_{align} + \{T_{step} + N_{shot} \times \\ &\quad t_{scan}(V_{scan})\} + T_{unload} \end{aligned} \quad \dots (15)$$

As described above so far, all the times except  
20 for  $T_{scan}(V_{scan})$  need not be regarded as functions of  $V_{scan}$ , and are constant values, and hence the time  $T$  required to process one wafer at the scanning velocity  $V_{scan.min}$  takes a minimum value. That is, the maximum number of wafers processed is set.

25 Therefore, the scanning velocity  $V_t$  at which the maximum number of wafers processed is set is expressed as

$$V_t = V_{\text{scan.min}} \quad \dots (16)$$

As described above, since the scanning velocity  $V$  must satisfy equations (6), (8), (10, and (11), the scanning velocity  $V$  at which the throughput is

5 substantially maximized is given by

$$V = \min(V_{\text{max}}, V_d, V_p, V_t)$$

where  $\min()$  is a function for obtaining a minimum value.

According to equations (12), (14), and (15), the relationship between the scanning velocity and the  
 10 throughput exhibits the form shown in Fig. 7A. Assume that  $V_{\text{max}}$ ,  $V_d$ ,  $V_p$ , and  $V_t$  have a relationship like that shown in Fig. 7A ( $V_t < V_p < V_{\text{max}} < V_d$ ). In this case, if the conventional method without any consideration given to the scanning velocity  $V_t$  at which the number  
 15 of wafers processed is maximized is used, exposure is performed at the scanning velocity  $V_p$  which is high and at which the synchronization error tends to become large, and the throughput at this time become  $TP_{V_p}$ . If the method of the present invention is used, exposure  
 20 is performed at the scanning velocity  $V_t$  which is lower than  $V_p$  and advantageous in terms of synchronization precision, and the throughput at this time is  $TP_{V_t}$ .

As is obvious from Fig. 7A, since  $TP_{V_p} \leq TP_{V_t}$ , the productivity can be improved.

25 (Second Embodiment)

The second embodiment of the present invention will be described. In this case, Figs. 3B and 5 show

the relationship between the shot layout on a wafer,  
the wafer stage velocity, and the mask stage velocity.

When a slit-like light beam moves from a shot  
area B to a shot area C, the wafer stage starts  
5 decelerating at exposure end time  $t_{B3}$  in Fig. 4. In  
this case, however, even after the exposure ends at  
time  $t_{B3}$ , the wafer stage moves at the same velocity  
as that in the exposure operation, and starts  
decelerating at time  $t_{B4}$  to decrease the velocity to 0  
10 at an approach start position for exposure of the shot  
area C. The wafer stage reaches the approach start  
position for exposure of the shot area C at time  $t_{B6}$   
( $t_{C0}$ ).

In this case, a length  $L$  that the wafer stage  
15 scans at a constant velocity in one scanning operation  
is expressed by  $L > L_y + W_s$  instead of  $L = L_y + W_s$ .  
The length  $L$  varies for each shot area, and a scanning  
velocity  $V_{scan.minB}$  in the shot area B is higher than a  
scanning velocity  $V_{scan.minA}$  that minimizes the time  
20 period from the start of scanning of the shot area A to  
the end of scanning.

In practice, a scanning velocity must be so  
determined as to satisfy equations (6), (8), and (10)  
as well. For this reason, a scanning velocity  $V_A$  that  
25 minimizes the time period from the start of scanning of  
the shot area A to the end of scanning while satisfying  
equations (6), (8), and (10) is given by

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$$V\_A = \min(V_{\max}, V_d, V_p, V_{\text{scan.minA}})$$

In the shot area B,

$$V\_B = \min(V_{\max}, V_d, V_p, V_{\text{scan.minB}})$$

Assume that Fig. 7B shows the relationship

5 between the scanning velocity and a time  $t(V_{\text{scan}})$  from  
the start of scanning of the shot area A to the end of  
scanning, and Fig. 7C shows the relationship between  
the scanning velocity and a time  $t(V_{\text{scan}})$  from the  
start of scanning of the shot area B to the end of  
10 scanning. In this case, the above scanning velocities  
 $V\_A$  and  $V\_B$  are respectively given by

$$V\_A = V_{\text{scan.minA}}$$

$$V\_B = V_p$$

and hence differ from each other.

15 If, therefore, the scanning velocity is changed  
in accordance with the length  $L$  that is scanned at a  
constant velocity in one scanning operation for each  
shot area, the time required for each shot area can be  
minimized. As a consequence, the throughput can be  
20 maximized.

In the case described above, the slit-like light  
beam moves from a given shot area to another shot area,  
which are equal in size but differ in their positions  
in the Y direction. However, the same applies to a  
25 case where shot areas have different sizes within a  
wafer, because the length  $L$  that is scanned at a  
constant velocity varies.

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In the above case, for example,  $\alpha_{\text{accel}}$ ,  $\alpha_{\text{decel}}$ , and  $t_{\text{settle}}$  are set to constant values within a wafer, and exposure is performed from the upper right shot area on the wafer in the order of  $S \rightarrow A \rightarrow B \rightarrow C \rightarrow \dots$

5 In addition, movement end times  $t_{A5}$  and  $t_{B5}$  in the non-scanning direction are set to be earlier than exposure start times  $t_{B2}$  and  $t_{C2}$  for the next shot area to prevent movement in the non-scanning direction from influencing the time  $T_{\text{scan}}$  required for scanning exposure.

10

Assume that a different exposure order is set, movement in the non-scanning direction or movement of the mask stage influences the time  $T_{\text{scan}}$  required for scanning exposure, and  $\alpha_{\text{accel}}$ ,  $\alpha_{\text{decel}}$ ,  $t_{\text{settle}}$ ,  $V_{\text{step}}$ , and the like vary within a wafer. In this case, if accelerations are determined in accordance with actual stage control in consideration of smooth velocity changes at P1 and P2 as shown in Fig. 6B instead of assuming the average accelerations  $\alpha_{\text{accel}}$  and  $\alpha_{\text{decel}}$  that abruptly change at P1 and P2 as shown in Fig. 6A, and the accelerations themselves are functions of a scanning velocity, the scanning velocity  $V_t$  at which the number of wafers processed is maximized is not necessarily given by equation (16).

15

20

25 In such a case, if representative values  $\alpha_{\text{accel}}$  and  $\alpha_{\text{decel}}$  within a wafer are used, a relationship similar to that represented by equation (16) is

established. Strictly speaking, the scanning velocity  $V_t$  at which the number of wafers processed is maximized can be expressed as a function of  $V_{scan.min}$  as follows:

$$V_t = g(V_{scan.min}) \quad \dots (17)$$

5 where  $g()$  is an arbitrary function.

The function  $g()$  may be actually obtained by one of the following methods. For example, scanning velocities  $V_{t.1}$ ,  $V_{t.2}$ ,  $V_{t.3}$ , ... at which the number of wafers processed is maximized are actually obtained  
10 under several conditions including the length  $L$  that is scanned at a constant velocity in one scanning operation, accelerations, and the like, and these velocities are approximated as a polynomial of  $V_{scan.min}$ . Alternatively, scanning velocities are  
15 determined as constant multiples of  $V_{scan.min}$  for the respective conditions and approximated in the form of a table.

According to another method, if an acceleration/deceleration pattern like that shown in  
20 Fig. 6A or 6B, including an exposure order and variations within a wafer, is known, a time  $T$  required to process one wafer can be calculated. In this case, a time  $T_{align}$  required for alignment and a time  $T_{unload}$  required for wafer recovery, which are regarded as  
25 constant values in the above description, may be accurately calculated as functions of a scanning velocity  $V_{scan}$ . If the time  $T$  required to process one

wafer is calculated in this manner, a scanning velocity  $V_t$  at which the number of wafers processed is maximized can be obtained by numerical calculation.

The above embodiments have exemplified the case  
5 where a pulse laser is used. Even if, however, a continuous light source like a mercury lamp is used, the scanning velocity  $V$  that maximizes the throughput can be obtained by the equation given below in the same manner as described above except that there is no need  
10 to consider a velocity  $V_p$  controlled with the minimum number of exposure pulses.

$$V = \min(V_{\max}, V_d, V_t)$$

The scanning velocity  $V$  for each shot in each shot area in the exposure apparatus according to each  
15 embodiment described above is displayed on a display (not shown).

(Embodiment of Semiconductor Production System)

A production system for producing a semiconductor device (semiconductor chip such as an IC or LSI, liquid  
20 crystal panel, CCD, thin-film magnetic head, micromachine, or the like) by using the exposure apparatus according to the present invention will be exemplified. A trouble remedy or periodic maintenance of a manufacturing apparatus installed in a  
25 semiconductor manufacturing factory, or maintenance service such as software distribution is performed by using a computer network outside the manufacturing



factory.

Fig. 8 shows the overall system cut out at a given angle. In Fig. 8, reference numeral 1101 denotes a business office of a vendor (apparatus supply  
5 manufacturer) which provides a semiconductor device manufacturing apparatus. Assumed examples of the manufacturing apparatus are semiconductor manufacturing apparatuses for various processes used in a semiconductor manufacturing factory, such as  
10 pre-process apparatuses (lithography apparatus including an exposure apparatus, resist processing apparatus, and etching apparatus, annealing apparatus, film formation apparatus, planarization apparatus, and the like) and post-process apparatuses (assembly  
15 apparatus, inspection apparatus, and the like). The business office 1101 comprises a host management system 1108 for providing a maintenance database for the manufacturing apparatus, a plurality of operation terminal computers 1110, and a LAN (Local Area Network)  
20 1109 which connects the host management system 1108 and computers 1110 to build an intranet. The host management system 1108 has a gateway for connecting the LAN 1109 to Internet 1105 as an external network of the business office, and a security function for limiting  
25 external accesses.

Reference numerals 1102 to 1104 denote manufacturing factories of the semiconductor

manufacturer as users of manufacturing apparatuses.

The manufacturing factories 1102 to 1104 may belong to different manufacturers or the same manufacturer (pre-process factory, post-process factory, and the

5 like). Each of the factories 1102 to 1104 is equipped with a plurality of manufacturing apparatuses 1106, a LAN (Local Area Network) 1111 which connects these apparatuses 1106 to construct an intranet, and a host management system 1107 serving as a monitoring  
10 apparatus for monitoring the operation status of each manufacturing apparatus 1106. The host management system 1107 in each of the factories 1102 to 1104 has a gateway for connecting the LAN 1111 in the factory to the Internet 1105 as an external network of the factory.  
15 Each factory can access the host management system 1108 of the vendor 1101 from the LAN 1111 via the Internet 1105. The security function of the host management system 1108 authorizes access of only a limited user. More specifically, the factory notifies the vendor via  
20 the Internet 1105 of status information (e.g., the symptom of a manufacturing apparatus in trouble) representing the operation status of each manufacturing apparatus 1106, and receives response information (e.g., information designating a remedy against the trouble,  
25 or remedy software or data) corresponding to the notification, or maintenance information such as the latest software or help information. Data

communication between the factories 1102 to 1104 and  
the vendor 1101 and data communication via the LAN 1111  
in each factory adopt a communication protocol (TCP/IP)  
generally used in the Internet. Instead of using the  
5 Internet as an external network of the factory, a  
dedicated network (e.g., ISDN) having high security  
which inhibits access of a third party can be adopted.  
Also the user may construct a database in addition to  
the one provided by the vendor and set the database on  
10 an external network, and the host management system may  
authorize access to the database from a plurality of  
user factories.

Fig. 9 is a view showing the concept of the  
overall system of this embodiment that is cut out at a  
15 different angle from Fig. 8. In the above example, a  
plurality of user factories having manufacturing  
apparatuses and the management system of the  
manufacturing apparatus vendor are connected via an  
external network, and production management of each  
20 factory or information of at least one manufacturing  
apparatus is communicated via the external network. In  
the example of Fig. 9, a factory having manufacturing  
apparatuses of a plurality of vendors and the  
management systems of the vendors for these  
25 manufacturing apparatuses are connected via the  
external network of the factory, and maintenance  
information of each manufacturing apparatus is

communicated. In Fig. 9, reference numeral 1201 denotes a manufacturing factory of a manufacturing apparatus user (semiconductor device manufacturer) where manufacturing apparatuses for various processes, e.g., an exposure apparatus 1202, resist processing apparatus 1203, and film formation apparatus 1204 are installed in the manufacturing line of the factory. Fig. 9 shows only one manufacturing factory 1201, but a plurality of factories are networked in practice. The respective apparatuses in the factory are connected to a LAN 1206 to build an intranet, and a host management system 1205 manages the operation of the manufacturing line.

The business offices of vendors (apparatus supply manufacturers) such as an exposure apparatus manufacturer 1210, resist processing apparatus manufacturer 1220, and film formation apparatus manufacturer 1230 comprise host management systems 1211, 1221, and 1231 for executing remote maintenance for the supplied apparatuses. Each host management system has a maintenance database and a gateway for an external network, as described above. The host management system 1205 for managing the apparatuses in the manufacturing factory of the user, and the management systems 1211, 1221, and 1231 of the vendors for the respective apparatuses are connected via the Internet or dedicated network serving as an external network

1200. If a trouble occurs in any one of a series of manufacturing apparatuses along the manufacturing line in this system, the operation of the manufacturing line stops. This trouble can be quickly solved by remote  
5 maintenance from the vendor of the apparatus in trouble via the Internet 1200. This can minimize the stop of the manufacturing line.

Each manufacturing apparatus in the semiconductor manufacturing factory comprises a display, a network  
10 interface, and a computer for executing network access software and apparatus operating software which are stored in a storage device. The storage device is a built-in memory, hard disk, or network file server. The network access software includes a dedicated or  
15 general-purpose web browser, and provides a user interface having a window as shown in Fig. 10 on the display. While referring to this window, the operator who manages manufacturing apparatuses in each factory inputs, in input items on the windows, pieces of  
20 information such as the type of manufacturing apparatus 1401, serial number 1402, object of trouble 1403, occurrence date 1404, degree of urgency 1405, symptom 1406, remedy 1407, and progress 1408. The pieces of input information are transmitted to the maintenance  
25 database via the Internet, and appropriate maintenance information is sent back from the maintenance database and displayed on the display. The user interface

provided by the web browser realizes hyperlink  
functions 1410 to 1412, as shown in Fig. 10. This  
allows the operator to access detailed information of  
each item, receive the latest-version software to be  
5 used for a manufacturing apparatus from a software  
library provided by a vendor, and receive an operation  
guide (help information) as a reference for the  
operator in the factory. Maintenance information  
provided by the maintenance database also includes  
10 information concerning the present invention described  
above. The software library also provides the latest  
software for implementing the present invention.

A semiconductor device manufacturing process  
using the above-described production system will be  
15 explained. Fig. 11 shows the flow of the whole  
manufacturing process of the semiconductor device. In  
step 1 (circuit design), a semiconductor device circuit  
is designed. In step 2 (mask formation), a mask having  
the designed circuit pattern is formed. In step 3  
20 (wafer manufacture), a wafer is manufactured by using a  
material such as silicon. In step 4 (wafer process)  
called a pre-process, an actual circuit is formed on  
the wafer by lithography using a prepared mask and the  
wafer. Step 5 (assembly) called a post-process is the  
25 step of forming a semiconductor chip by using the wafer  
manufactured in step 4, and includes an assembly  
process (dicing and bonding) and packaging process



after etching is removed. These steps are repeated to form multiple circuit patterns on the wafer. A manufacturing apparatus used in each step undergoes maintenance by the remote maintenance system, which prevents a trouble in advance. Even if a trouble occurs, the manufacturing apparatus can be quickly recovered. The productivity of the semiconductor device can be increased in comparison with the prior art.

10 According to the present invention, there are provided an exposure apparatus which can perform scanning exposure with a maximum possible throughput by determining a scanning velocity in consideration of the maximum scanning velocity determined from the performance of a stage control system, including structural and mechanical performance, the scanning velocity determined from an exposure amount, the scanning velocity determined from the minimum number of exposure pulses, and the scanning velocity that maximizes the number of substrates such as wafers to be processed, and a device manufacturing method using the exposure apparatus. This makes it possible to increase the throughput while satisfying various constraint conditions.

25 In addition, the scanning velocity  $V_t$  at which the number of substrates processed per unit time is maximized, which is determined from a transfer pattern



size, the layout on the transfer pattern, a transfer means, a master scanning means, a substrate scanning means, and a positioning means is calculated in advance by simulation based on a transfer pattern size, the  
5 layout on the transfer pattern, and conditions in the transfer means, master scanning means, substrate stage scanning means, and positioning means, or is changed for each transfer pattern in accordance with a transfer pattern size and the layout of the transfer pattern on  
10 a substrate. The throughput can be further increased by changing the scanning velocity for each shot area to be exposed in accordance with the length that is scanned at a constant velocity in one scanning operation.

15 As many apparently widely different embodiments of the present invention can be made without departing from the spirit and scope thereof, it is to be understood that the invention is not limited to the specific embodiments thereof except as defined in the  
20 appended claims.